

EXERCISES ON TENSOR ALGEBRA

Problem 1. Consider the tensor $\mathbf{F} = 3\mathbf{e}_1 \otimes \mathbf{e}_1 - 2\mathbf{e}_1 \otimes \mathbf{e}_2 - \mathbf{e}_2 \otimes \mathbf{e}_2 + 2\mathbf{e}_2 \otimes \mathbf{e}_3 - \mathbf{e}_3 \otimes \mathbf{e}_1$.

- (1) Compute the determinant $\det \mathbf{F}$ and the trace $\text{tr} \mathbf{F}$.
- (2) What is the image under \mathbf{F} of the vector $\mathbf{u} := 3\mathbf{e}_1 - \mathbf{e}_2 + 2\mathbf{e}_3$?
- (3) Decompose \mathbf{F} into its symmetric part $\text{sym} \mathbf{F}$ and its skew-symmetric part $\text{skw} \mathbf{F}$.
- (4) What is the axial vector of $\text{skw} \mathbf{F}$?
- (5) Write the inverse tensor \mathbf{F}^{-1} and the adjugate tensor \mathbf{F}^* .
- (6) What is the area dilation factor of \mathbf{F} for surfaces orthogonal to \mathbf{e}_2 ?

Solution:

- (1) $\det \mathbf{F} = 4$ and $\text{tr} \mathbf{F} = 2$
- (2) $\mathbf{F}\mathbf{u} = 11\mathbf{e}_1 + 5\mathbf{e}_2 - 3\mathbf{e}_3$
- (3) $\text{sym} \mathbf{F} = 3\mathbf{e}_1 \otimes \mathbf{e}_1 - \mathbf{e}_1 \otimes \mathbf{e}_2 - \frac{1}{2}\mathbf{e}_1 \otimes \mathbf{e}_3 - \mathbf{e}_2 \otimes \mathbf{e}_1 - \mathbf{e}_2 \otimes \mathbf{e}_2 + \mathbf{e}_2 \otimes \mathbf{e}_3 - \frac{1}{2}\mathbf{e}_3 \otimes \mathbf{e}_1 + \mathbf{e}_3 \otimes \mathbf{e}_2$
and $\text{skw} \mathbf{F} = -\mathbf{e}_1 \otimes \mathbf{e}_2 + \frac{1}{2}\mathbf{e}_1 \otimes \mathbf{e}_3 + \mathbf{e}_2 \otimes \mathbf{e}_1 + \mathbf{e}_2 \otimes \mathbf{e}_3 - \frac{1}{2}\mathbf{e}_3 \otimes \mathbf{e}_1 - \mathbf{e}_3 \otimes \mathbf{e}_2$
- (4) $\mathbf{w}(\text{skw} \mathbf{F}) = -\mathbf{e}_1 + \frac{1}{2}\mathbf{e}_2 + \mathbf{e}_3$
- (5) $\mathbf{F}^{-1} = -\mathbf{e}_1 \otimes \mathbf{e}_3 - \frac{1}{2}\mathbf{e}_2 \otimes \mathbf{e}_1 - \frac{3}{2}\mathbf{e}_2 \otimes \mathbf{e}_3 - \frac{1}{4}\mathbf{e}_3 \otimes \mathbf{e}_1 + \frac{1}{2}\mathbf{e}_3 \otimes \mathbf{e}_2 - \frac{3}{4}\mathbf{e}_3 \otimes \mathbf{e}_3$
and $\mathbf{F}^* = -4\mathbf{e}_3 \otimes \mathbf{e}_1 - 2\mathbf{e}_1 \otimes \mathbf{e}_2 - 6\mathbf{e}_3 \otimes \mathbf{e}_2 - \mathbf{e}_1 \otimes \mathbf{e}_3 + 2\mathbf{e}_2 \otimes \mathbf{e}_3 - 3\mathbf{e}_3 \otimes \mathbf{e}_3$
- (6) $|\mathbf{F}^*\mathbf{e}_2| = 2\sqrt{10}$

Problem 2. Consider the tensor $\mathbf{F} = -\mathbf{e}_1 \otimes \mathbf{e}_1 + \mathbf{e}_1 \otimes \mathbf{e}_3 + 2\mathbf{e}_2 \otimes \mathbf{e}_1 - \mathbf{e}_2 \otimes \mathbf{e}_2 + 2\mathbf{e}_3 \otimes \mathbf{e}_2 - \mathbf{e}_3 \otimes \mathbf{e}_3$.

- (1) Compute the determinant $\det \mathbf{F}$ and the trace $\text{tr} \mathbf{F}$.
- (2) What is the image under \mathbf{F} of the vector $\mathbf{u} := \mathbf{e}_1 - \mathbf{e}_2 + \mathbf{e}_3$?
- (3) Decompose \mathbf{F} into its symmetric part $\text{sym} \mathbf{F}$ and its skew-symmetric part $\text{skw} \mathbf{F}$.
- (4) What is the axial vector of $\text{skw} \mathbf{F}$?
- (5) Write the inverse tensor \mathbf{F}^{-1} and the adjugate tensor \mathbf{F}^* .
- (6) What is the area dilation factor of \mathbf{F} for surfaces orthogonal to \mathbf{e}_3 ?

Solution:

(1) $\det \mathbf{F} = 3$ and $\text{tr} \mathbf{F} = -3$

(2) $\mathbf{F}\mathbf{u} = 3\mathbf{e}_2 - 3\mathbf{e}_3$

(3) $\text{sym} \mathbf{F} = -\mathbf{e}_1 \otimes \mathbf{e}_1 + \mathbf{e}_1 \otimes \mathbf{e}_2 + \frac{1}{2}\mathbf{e}_1 \otimes \mathbf{e}_3 + \mathbf{e}_2 \otimes \mathbf{e}_1 - \mathbf{e}_2 \otimes \mathbf{e}_2 + \mathbf{e}_2 \otimes \mathbf{e}_3 + \frac{1}{2}\mathbf{e}_3 \otimes \mathbf{e}_1 + \mathbf{e}_3 \otimes \mathbf{e}_2 - \mathbf{e}_3 \otimes \mathbf{e}_3$
 and $\text{skw} \mathbf{F} = -\mathbf{e}_1 \otimes \mathbf{e}_2 + \frac{1}{2}\mathbf{e}_1 \otimes \mathbf{e}_3 + \mathbf{e}_2 \otimes \mathbf{e}_1 - \mathbf{e}_2 \otimes \mathbf{e}_3 - \frac{1}{2}\mathbf{e}_3 \otimes \mathbf{e}_1 + \mathbf{e}_3 \otimes \mathbf{e}_2$

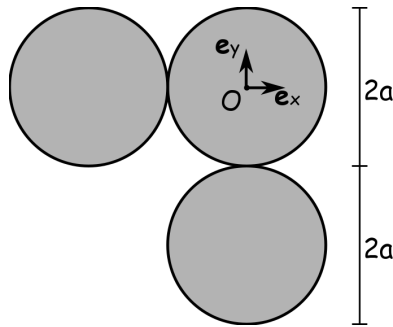
(4) $\mathbf{w}(\text{skw} \mathbf{F}) = \mathbf{e}_1 + \frac{1}{2}\mathbf{e}_2 + \mathbf{e}_3$

(5) $\mathbf{F}^{-1} = \frac{1}{3}\mathbf{e}_1 \otimes \mathbf{e}_1 + \frac{2}{3}\mathbf{e}_1 \otimes \mathbf{e}_2 + \frac{1}{3}\mathbf{e}_1 \otimes \mathbf{e}_3 + \frac{2}{3}\mathbf{e}_2 \otimes \mathbf{e}_1 + \frac{1}{3}\mathbf{e}_2 \otimes \mathbf{e}_2 + \frac{2}{3}\mathbf{e}_2 \otimes \mathbf{e}_3 + \frac{4}{3}\mathbf{e}_3 \otimes \mathbf{e}_1 + \frac{2}{3}\mathbf{e}_3 \otimes \mathbf{e}_2 + \frac{1}{3}\mathbf{e}_3 \otimes \mathbf{e}_3$
 and $\mathbf{F}^* = \mathbf{e}_1 \otimes \mathbf{e}_1 + 2\mathbf{e}_2 \otimes \mathbf{e}_1 + \mathbf{e}_3 \otimes \mathbf{e}_1 + 2\mathbf{e}_1 \otimes \mathbf{e}_2 + \mathbf{e}_2 \otimes \mathbf{e}_2 + 2\mathbf{e}_3 \otimes \mathbf{e}_2 + 4\mathbf{e}_1 \otimes \mathbf{e}_3 + 2\mathbf{e}_2 \otimes \mathbf{e}_3 + \mathbf{e}_3 \otimes \mathbf{e}_3$

(6) $|\mathbf{F}^* \mathbf{e}_3| = \sqrt{21}$

EXERCISES ON INERTIA

Problem 3. Suppose the following grey body to be in \mathbb{R}^3 and to have uniform mass density ρ :



- (1) Write the vector position $C - O$ of the center of mass of the body.
- (2) Write a principal basis for the central tensor of inertia \mathbf{I}_C (that is: a basis of \mathbb{R}^3 , made of principal versors of the tensor of inertia of the body at C).
- (3) Write the central tensor of inertia \mathbf{I}_C of the body.
- (4) Write the tensor of inertia \mathbf{I}_O of the body.

Solution:

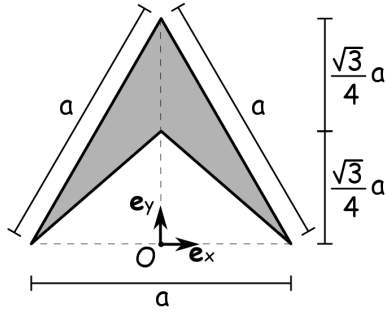
$$(1) \quad C - O = -\frac{2}{3}a(\mathbf{e}_x + \mathbf{e}_y)$$

$$(2) \quad \text{A principal basis is } (\mathbf{e}_1, \mathbf{e}_2, \mathbf{e}_3), \text{ with } \mathbf{e}_1 := \frac{\sqrt{2}}{2}(\mathbf{e}_x + \mathbf{e}_y), \mathbf{e}_2 := \frac{\sqrt{2}}{2}(-\mathbf{e}_x + \mathbf{e}_y) \\ \text{and } \mathbf{e}_3 := \mathbf{e}_x \times \mathbf{e}_y$$

$$(3) \quad \mathbf{I}_C = \frac{19}{4}\pi\rho a^4\mathbf{e}_1 \otimes \mathbf{e}_1 + \frac{25}{12}\pi\rho a^4\mathbf{e}_2 \otimes \mathbf{e}_2 + \frac{41}{6}\pi\rho a^4\mathbf{e}_3 \otimes \mathbf{e}_3$$

$$(4) \quad \mathbf{I}_O = \frac{19}{4}\pi\rho a^4\mathbf{e}_1 \otimes \mathbf{e}_1 + \frac{257}{108}\pi\rho a^4\mathbf{e}_2 \otimes \mathbf{e}_2 + \frac{385}{54}\pi\rho a^4\mathbf{e}_3 \otimes \mathbf{e}_3$$

Problem 4. Suppose the following grey body to be in \mathbb{R}^3 and to have uniform mass density ρ :



- (1) Write the vector position $C - O$ of the center of mass of the body.
- (2) Write a principal basis for the central tensor of inertia \mathbf{I}_C (that is: a basis of \mathbb{R}^3 , made of principal versors of the tensor of inertia of the body at C).
- (3) Write the central tensor of inertia \mathbf{I}_C of the body.
- (4) Write the tensor of inertia \mathbf{I}_O of the body.

Solution:

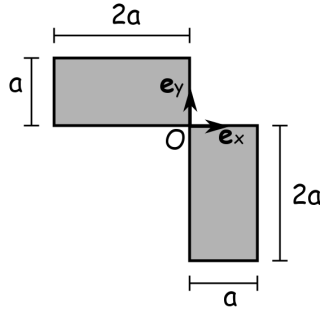
$$(1) C - O = \frac{\sqrt{3}}{4} a \mathbf{e}_y$$

$$(2) \text{ A principal basis is } (\mathbf{e}_x, \mathbf{e}_y, \mathbf{e}_z), \text{ with } \mathbf{e}_z := \mathbf{e}_x \times \mathbf{e}_y$$

$$(3) \mathbf{I}_C = \frac{\sqrt{3}}{256} \rho a^4 \mathbf{e}_1 \otimes \mathbf{e}_1 + \frac{\sqrt{3}}{192} \rho a^4 \mathbf{e}_2 \otimes \mathbf{e}_2 + \frac{7\sqrt{3}}{768} \rho a^4 \mathbf{e}_3 \otimes \mathbf{e}_3$$

$$(4) \mathbf{I}_O = \frac{7\sqrt{3}}{256} \rho a^4 \mathbf{e}_1 \otimes \mathbf{e}_1 + \frac{\sqrt{3}}{192} \rho a^4 \mathbf{e}_2 \otimes \mathbf{e}_2 + \frac{25\sqrt{3}}{768} \rho a^4 \mathbf{e}_3 \otimes \mathbf{e}_3$$

Problem 5. Suppose the following grey body to be in \mathbb{R}^3 and to have uniform mass density ρ :



- (1) Write the vector position $C - O$ of the center of mass of the body.
- (2) Write a principal basis for the central tensor of inertia \mathbf{I}_C (that is: a basis of \mathbb{R}^3 , made of principal versors of the tensor of inertia of the body at C).
- (3) Write the central tensor of inertia \mathbf{I}_C of the body.
- (4) Write the tensor of inertia \mathbf{I}_O of the body.

Solution:

$$(1) \quad C - O = -\frac{1}{4}a(\mathbf{e}_x + \mathbf{e}_y)$$

$$(2) \quad \text{A principal basis is } (\mathbf{e}_1, \mathbf{e}_2, \mathbf{e}_3), \text{ with } \mathbf{e}_1 := \frac{\sqrt{2}}{2}(\mathbf{e}_x + \mathbf{e}_y), \mathbf{e}_2 := \frac{\sqrt{2}}{2}(-\mathbf{e}_x + \mathbf{e}_y) \\ \text{and } \mathbf{e}_3 := \mathbf{e}_x \times \mathbf{e}_y$$

$$(3) \quad \mathbf{I}_C = \frac{37}{12}\rho a^4(\mathbf{e}_x \otimes \mathbf{e}_x + \mathbf{e}_y \otimes \mathbf{e}_y + 2\mathbf{e}_z \otimes \mathbf{e}_z) + \frac{9}{4}\rho a^4(\mathbf{e}_x \otimes \mathbf{e}_y + \mathbf{e}_y \otimes \mathbf{e}_x)$$

$$(4) \quad \mathbf{I}_O = \frac{10}{3}\rho a^4(\mathbf{e}_x \otimes \mathbf{e}_x + \mathbf{e}_y \otimes \mathbf{e}_y + 2\mathbf{e}_z \otimes \mathbf{e}_z) + 2\rho a^4(\mathbf{e}_x \otimes \mathbf{e}_y + \mathbf{e}_y \otimes \mathbf{e}_x)$$

EXERCISES ON CURVES

Problem 6. Consider the curve defined as follows:

$$P(\vartheta) := \left(\frac{\sqrt{14}}{4}\vartheta, \frac{1}{6}(\sqrt{1+\vartheta})^3, \frac{1}{6}(\sqrt{1-\vartheta})^3 \right) \quad \text{with } \vartheta \in \left[-\frac{1}{2}, \frac{1}{2} \right]$$

- (1) Write the arc-length parameter s of the curve.
- (2) Find the length L of the curve in the interval $\left[-\frac{1}{2}, \frac{1}{2} \right]$.
- (3) Write the tangent vector \mathbf{t} , the normal vector \mathbf{n} and the binormal vector \mathbf{b} of the curve for $\vartheta \in \left[-\frac{1}{2}, \frac{1}{2} \right]$.
- (4) Compute the curvature c and the torsion τ of the curve for $\vartheta \in \left[-\frac{1}{2}, \frac{1}{2} \right]$.

Solution:

(1) $s = \vartheta$

(2) $L = 1$

(3) $\mathbf{t}(\vartheta) = \left(\frac{\sqrt{14}}{4}, \frac{\sqrt{1+\vartheta}}{4}, -\frac{\sqrt{1-\vartheta}}{4} \right)$, $\mathbf{n}(\vartheta) = \left(0, \frac{\sqrt{1-\vartheta}}{\sqrt{2}}, \frac{\sqrt{1+\vartheta}}{\sqrt{2}} \right)$ and

$$\mathbf{b}(\vartheta) = \left(\frac{\sqrt{2}}{4}, -\frac{\sqrt{7}\sqrt{1+\vartheta}}{4}, \frac{\sqrt{7}\sqrt{1-\vartheta}}{4} \right)$$

(4) $c(\vartheta) = \frac{\sqrt{2}}{8\sqrt{1-\vartheta^2}}$ and $\tau(\vartheta) = -\frac{\sqrt{14}}{8\sqrt{1-\vartheta^2}}$

Problem 7. Consider the curve defined as follows:

$$P(\vartheta) := \left(\vartheta, -\frac{\sqrt{2}}{2}\vartheta^2, \frac{\sqrt{2}}{2}\vartheta^2 \right) \quad \text{with } \vartheta \in \mathbb{R}$$

- (1) Write the tangent vector \mathbf{t} , the normal vector \mathbf{n} and the binormal vector \mathbf{b} of the curve for $\vartheta \in \mathbb{R}$.
- (2) Compute the curvature c and the torsion τ of the curve for $\vartheta \in \mathbb{R}$.

Solution:

- (1) $\mathbf{t}(\vartheta) = \frac{1}{\sqrt{4\vartheta^2 + 1}} (1, -\sqrt{2}\vartheta, \sqrt{2}\vartheta)$, $\mathbf{n}(\vartheta) = \frac{1}{\sqrt{4\vartheta^2 + 1}} (-2\vartheta, -\sqrt{2}, \sqrt{2})$ and
 $\mathbf{b}(\vartheta) = \frac{\sqrt{2}}{2} (0, -1, -1)$
- (2) $c(\vartheta) = \frac{2}{(\sqrt{4\vartheta^2 + 1})^3}$ and $\tau(\vartheta) = 0$

Problem 8. Consider the curve defined as follows:

$$P(\vartheta) := \left(\vartheta, \vartheta^2, \frac{2}{3}\vartheta^3 \right) \quad \text{with } \vartheta \in \mathbb{R}$$

- (1) Find the length L of the curve in the interval $[-1, 3]$.
- (2) Write the tangent vector \mathbf{t} , the normal vector \mathbf{n} and the binormal vector \mathbf{b} of the curve for $\vartheta \in \mathbb{R}$.
- (3) Compute the curvature c and the torsion τ of the curve for $\vartheta \in \mathbb{R}$.

Solution:

$$(1) \quad L = \frac{68}{3}$$

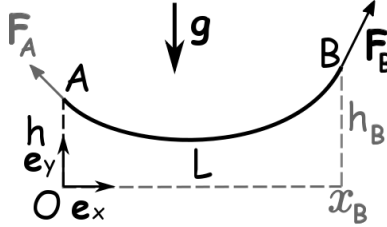
$$(2) \quad \mathbf{t}(\vartheta) = \frac{1}{2\vartheta^2 + 1} (1, 2\vartheta, 2\vartheta^2), \quad \mathbf{n}(\vartheta) = \frac{1}{2\vartheta^2 + 1} (-2\vartheta, 1 - 2\vartheta^2, 2\vartheta) \quad \text{and}$$

$$\mathbf{b}(\vartheta) = \frac{1}{2\vartheta^2 + 1} (2\vartheta^2, -2\vartheta, 1)$$

$$(3) \quad c(\vartheta) = \frac{2}{(2\vartheta^2 + 1)^2} \quad \text{and} \quad \tau(\vartheta) = -\frac{2}{(2\vartheta^2 + 1)^2}$$

EXERCISES ON CABLES

Problem 9. A cable with length L and linear mass density λ is hung in A at height h . At B a force $\mathbf{F}_B = \mathbf{e}_x + \frac{2}{3}\lambda g L \mathbf{e}_y$ is exerted on the cable, as shown in the following picture:



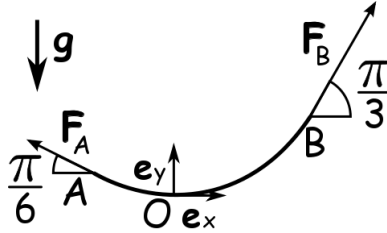
Assume that the only distributed force acting on the cable is due to the gravitational acceleration $\mathbf{g} = -g\mathbf{e}_y$.

- (1) Let $y(x)$ be the function that describes the shape of the cable. What is the condition for $y(0)$, at equilibrium?
- (2) Let $T(x)$ be the function that describes the tension of the cable, and let $\mathbf{t}(x)$ be the tangent vector to the shape of the cable. What is the condition that involves both the tension and the tangent at the point B , at equilibrium?
- (3) Write the function $y(x)$.
- (4) What is the height h_B of the point B at equilibrium?
- (5) For which value of x the tension is minimal?
- (6) What is the reactive force \mathbf{F}_A the cable is subjected to at A ?

Solution:

- (1) $y(0) = h$
- (2) $T(x_B)\mathbf{t}(x_B) = \mathbf{e}_x + \frac{2}{3}\lambda g L \mathbf{e}_y$
- (3) $y(x) = \frac{1}{\lambda g} \cosh\left(\lambda g x - \operatorname{asinh}\left(\frac{\lambda g L}{3}\right)\right) + h - \frac{1}{\lambda g} \cosh\left(\operatorname{asinh}\left(\frac{\lambda g L}{3}\right)\right)$
- (4) $h_B = \frac{1}{\lambda g} \left(\cosh\left(\operatorname{asinh}\left(\frac{2\lambda g L}{3}\right)\right) - \cosh\left(\operatorname{asinh}\left(\frac{\lambda g L}{3}\right)\right) \right) + h$
- (5) $x = \frac{1}{\lambda g} \operatorname{asinh}\left(\frac{\lambda g L}{3}\right)$
- (6) $\mathbf{F}_A = -\mathbf{e}_x + \frac{1}{3}\lambda g L \mathbf{e}_y$

Problem 10. A cable with linear mass density $\lambda = \frac{2p}{g}$ is subjected in A and B respectively to two forces \mathbf{F}_A and \mathbf{F}_B . The force \mathbf{F}_A makes an angle $\frac{\pi}{6}$ with the horizontal direction \mathbf{e}_x and the force \mathbf{F}_B makes an angle $\frac{\pi}{3}$ with the horizontal direction \mathbf{e}_x , as shown in the following picture:



The norm of the force \mathbf{F}_B is $|\mathbf{F}_B| = 3pl$, and the only distributed force acting on the cable is due to the gravitational acceleration $\mathbf{g} = -g\mathbf{e}_y$. Consider a reference system centered at the point O of minimal tension (as in the picture: $x_O = 0$ and $y_O = 0$).

- (1) Let $y(x)$ be the function that describes the shape of the cable. What are the conditions for $y(0)$ and $\dot{y}(0)$, at equilibrium?
- (2) Let $T(x)$ be the function that describes the tension of the cable, and let $\mathbf{t}(x)$ be the tangent versor to the shape of the cable. What is the condition that involves both the tension and the tangent at the point B , at equilibrium?
- (3) Write the function $y(x)$.
- (4) Write the vector $A - O$ and $B - O$.
- (5) What is the length L of the cable?

Solution:

$$(1) \quad y(0) = 0 \text{ and } \dot{y}(0) = 0$$

$$(2) \quad T(x_B)\mathbf{t}(x_B) = \mathbf{F}_B = \frac{3}{2}pl\mathbf{e}_x + \frac{3\sqrt{3}}{2}pl\mathbf{e}_y$$

$$(3) \quad y(x) = \frac{3}{4}l \left(\cosh\left(\frac{4}{3l}x\right) - 1 \right)$$

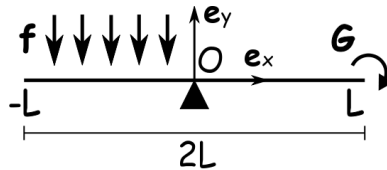
$$(4) \quad A - O = -\frac{3l}{4} \operatorname{asinh}\left(\frac{1}{\sqrt{3}}\right) \mathbf{e}_x + \frac{3l}{4} \left(\frac{2}{\sqrt{3}} - 1 \right) \mathbf{e}_y$$

$$\text{and } B - O = \frac{3l}{4} \operatorname{asinh}(\sqrt{3}) \mathbf{e}_x + \frac{3l}{4} \mathbf{e}_y$$

$$(5) \quad L = \sqrt{3}l$$

EXERCISES ON BEAMS

Problem 11. A uniformly elastic beam with $EI_2 = B$ and with length $2L$ is simply supported at its middle point O . The first half of the beam ($s \in [-L, 0]$) is subjected to a distributed force with density $\mathbf{f} = -f\mathbf{e}_y$ ($f > 0$) and a couple force $\mathbf{G} = G\mathbf{e}_z$ is exerted on the second end ($s = L$) of the beam, as shown in the following picture:



(Recall: the simple support exerts on the beam a reactive force \mathbf{F}_O only, and \mathbf{F}_O is orthogonal to the center line of the beam at O).

- (1) At equilibrium, what is the reactive force \mathbf{F}_O exerted on the beam and what is the relation between G and f ? (Hint: use the total balance of forces acting on the beam and the total balance of torques at $s = L$).
- (2) Let $P(s) = (x(s), y(s))$ be the curve that describes the shape of the beam at equilibrium, $\varphi(s)$ be the stress force at equilibrium and $\vartheta(s)$ be the angle between \mathbf{e}_x and the tangent to $P(s)$ at equilibrium. What are the boundary conditions for $y(s)$, $\varphi(s)$ and $\vartheta(s)$ at the ends $s = -L$ and $s = L$?
- (3) Write the conditions for $y(0)$ and $\vartheta(0)$.
- (4) Write the function $y(x)$ which represents the shape of the beam at equilibrium, in case of small deflections.
- (5) What is the maximum deflection $y_{\max} := \max\{|y(x)|\}$ of the beam, and for which values of x is this attained?
- (6) What is the maximum slope $\vartheta_{\max} := \max\{|\vartheta(x)|\}$ of the beam, and for which values of x is this attained?
- (7) What is the condition on the value of f that makes the small deflections approximation viable?

Solution:

(1) $\mathbf{F}_O = fL\mathbf{e}_y$ and $G = -\frac{1}{2}fL^2$

(2) $\vartheta'(-L) = 0$, $\vartheta'(L) = -\frac{fL^2}{2B}$, $\varphi(-L) = \mathbf{0}$ and $\varphi(L) = \mathbf{0}$

(3) $y(0) = 0$ and $\vartheta(0) = 0$

(4)
$$\begin{cases} y(x) = -\frac{f}{24B}x^2(x^2 + 4Lx + 6L^2) & x \in [-L, 0] \\ y(x) = -\frac{f}{4B}L^2x^2 & x \in [0, L] \end{cases}$$

(5) $y_{\max} = |y(L)| = \frac{fL^4}{4B}$

(6) $\vartheta_{\max} = |\vartheta(L)| = \frac{fL^3}{2B}$

(7) $f \ll \frac{2B}{L^3}$

Problem 12. A uniformly elastic beam with $EI_2 = B$ and with length L is clamped at one end and supported by a smooth disk of radius R at the other end, as shown in the following picture:



(Recall: the disk exerts a reactive force that is directed radially outward and orthogonal to the beam at the contact point).

- (1) Let $P(s) = (x(s), y(s))$ be the curve that describes the shape of the beam at equilibrium and $\vartheta(s)$ be the angle between \mathbf{e}_x and the tangent to $P(s)$ at equilibrium. What are the boundary conditions for $y(s)$, $\vartheta(s)$ and $\vartheta'(s)$ at the ends $s = 0$ and $s = L$?
- (2) Write the balance equations for forces and torques at equilibrium at the generic point s .
- (3) Write the function $y(x)$ which represents the shape of the beam at equilibrium, in case of small deflections.
- (4) What is the maximum deflection $y_{\max} := \max\{|y(x)|\}$ of the beam, and for which values of x is this attained?
- (5) What is the maximum slope $\vartheta_{\max} := \max\{|\vartheta(x)|\}$ of the beam, and for which values of x is this attained?
- (6) What is the condition on the radius R that makes the small deflections approximation viable?

Solution:

- (1) $y(0) = 0$, $\vartheta(0) = 0$, $y(L) = R \cos(\vartheta(L))$ and $\vartheta'(L) = 0$
- (2) $\varphi'(s) = \mathbf{0}$ and $(B\vartheta''(s) + F \cos(\vartheta(L)) \cos(\vartheta(s)) + F \sin(\vartheta(L)) \sin(\vartheta(s)))\mathbf{e}_z = \mathbf{0}$, with $F = |\mathbf{F}_L|$.
- (3) $y(x) = \frac{R}{2L^3}x^2(3L - x)$
- (4) $y_{\max} = y(L) = R$
- (5) $\vartheta_{\max} = \vartheta(L) = \frac{3R}{2L}$
- (6) $R \ll \frac{2}{3}L$